

22607

23124

4 Hours / 70 Marks

Seat No.

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- Instructions :**
- (1) All Questions are *compulsory*.
 - (2) Illustrate your answers with neat sketches wherever necessary.
 - (3) Figures to the right indicate full marks.
 - (4) Assume suitable data, if necessary.
 - (5) Use of Non-programmable Electronic Pocket Calculator is permissible.

Marks

1. Attempt any FIVE of the following :

10

- (a) Draw neat sketches of any four steel sections used as tension member.
- (b) Calculate effective length of a 6 m long column with both ends are fixed.
- (c) State the conditions of formation of Flanged beams.
- (d) Enumerate any two types of staircase, spanning longitudinally.
- (e) State live load on staircase of different types of buildings as per IS code.
- (f) Calculate effective span of a flight of a dog-legged stair supported by 230 mm wide beams at the end of landings. Rise is 150 mm while tread width is 300 mm. Width of landing is 1 m.
- (g) State IS recommendations about pitch of spiral ties in a circular column.

2. Attempt any THREE of the following :

12

- (a) Explain with sketches three modes of failure of an axial tension member.
- (b) Calculate effective flange width for a T beam if clear span of beam is 5.75 m, width of supports = 300 mm each, spacing of beams 2.5 m c/c, width of web = 250 mm and slab thickness = 100 mm.
- (c) Draw neat sketch of a circular column having spiral tie. State IS provisions regarding pitch of spiral.
- (d) State reasons for designing any column considering certain minimum eccentricity. State expression to calculate e_{\min} .



3. Attempt any TWO of the following :

12

- (a) A single angle of $100 \times 100 \times 10$ tie member is connected to a 12 mm thick gusset plate with 4 bolts of 18 mm diameter (with pitch of 60 mm and gauge of 40 mm). Determine block shear strength only of given tension member. Take $f_y = 250$ MPa and $f_u = 410$ MPa.
- (b) Design a suitable angle section as a tie member in a truss to carry factored load of 250 kN. Use double angle section connected back to back on both sides of 10 mm thick gusset plate by means of 4 bolts of 18 mm dia. in one line. (check of block shear not required)

Given $\alpha = 0.8$, $f_y = 250$ MPa, $f_u = 410$ MPa

Available Sections Gross Area (mm²)

ISA $90 \times 60 \times 6$	865
ISA $100 \times 75 \times 6$	1014
ISA $120 \times 80 \times 8$	1550

- (c) In a roof truss, a discontinuous strut of 2.5 m long consists of a Double angle section $100 \times 100 \times 6$ mm back to back on same sides of 8 mm thick gusset plate connected with 2 bolts of 16 mm diameter. Calculate safe load carried by strut.

Assume – Properties of ISA $100 \times 100 \times 6$ mm is as ; Area = 1167 mm²

$C_{xx} = C_{yy} = 26.7$ mm, $I_{xx} = I_{yy} = 111 \times 10^4$ mm⁴, $f_y = 250$ N/mm²

KL/r	:	80	90	100	110	120	130
f_{cd} (N/mm²)	:	136	121	107	94.6	83.7	74.6

4. Attempt any TWO of the following :

12

- (a) State the functions of lacing and battening. Draw diagram showing double lacing system. Also state general requirements for lacing as per IS 800.
- (b) Design a discontinuous rafter using double angle on opposite sides of G.P. to carry factored compressive load of 300 kN. c/c length is 2.35 m between welds on 12 mm thick gusset plate. Available sections are as follows :

Section	Area (mm ²)	I_{yy} (mm ⁴)	C_{yy} (mm)
ISA $90 \times 60 \times 8$	1137	32×10^4	14
ISA $80 \times 50 \times 10$	1202	75×10^4	13
ISA $90 \times 60 \times 10$	1401	111×10^4	15

- (c) Calculate the ultimate moment capacity of a beam 250×350 mm (effective) if it is reinforced with 4 – 16 mm diameter bars in tension zone and 3 – 12 mm diameter bars in compression zone, each at an effective cover of 40 mm. Assume M25 concrete and Fe500 steel is used. Take $f_{sc} = 355$ N/mm².

5. Attempt any TWO of the following :

12

- (a) A simply supported beam having effective span 5 m is to carry working UDL of 62 kN/m. Limiting section of RCC beam is 300 mm \times 400 mm (effective). Calculate area of steel required. Use M20 concrete and Fe415 steel. Assume $f_{sc} = 335$ N/mm².
- (b) Draw strain and stress block diagram for a doubly reinforced RC beam. Mark all important parameters and corresponding lever arms.
- (c) Calculate ultimate moment of resistance of a T beam having flange width 1100 mm, depth of slab 120 mm, effective depth of beam 500 mm, width of web 230 mm. Beam is reinforced with 4 numbers of 12 mm diameter bars. Assume M20 concrete and Fe415 steel.

6. Attempt any TWO of the following :

12

- (a) A simply supported singly reinforced flanged beam having effective span 6 m with flange width 2.2 m embedded in slab of 125 mm thick carries total working load of 60 kN/m. Calculate area of reinforcement at tension side. Assume effective depth of beam as 450 mm. M25 concrete and Fe415 steel are used.
- (b) Design dog legged stair case for residential building for floor to floor height 3 m, rise 150 mm, tread 250 mm with 1 m landings on both side. Assume M20 concrete and Fe415 steel. Flight is supported by beams at the end of landing.
- (c) Design a RC column footing for an axially loaded square column 450 mm \times 450 mm.
It carries a factored load of 1500 kN. Safe bearing capacity of soil is 250 kN/m². Use bending moment criteria only. Use M20 grade concrete & Fe415 steel.

IS : 800-2007 Equations (Formula Sheet)

$$V_{nsb} = \left(\frac{f_u}{\sqrt{3}} \right) (n_n A_{nb} + n_s A_{sb}), \quad V_{dsb} = \frac{V_{nsb}}{\gamma_{mb}}, \quad V_{dpb} = \frac{V_{npb}}{\gamma_{mb}},$$

$$T_{dg} = \frac{A_g f_y}{\gamma_{m0}}, \quad V_{npb} = 2.5 k_b d t f_u$$

$$T_{dn} = \frac{0.9 A_{nc} f_u}{\gamma_{m1}} + \beta \frac{A_{go} f_y}{\gamma_{m0}} \text{ where } \beta = 1.4 - 0.076 (w/t) (f_y/f_u) (bs/Lc) \leq \left(\frac{f_u \gamma_{m0}}{f_y \gamma_{m1}} \right) \geq 0.7$$

$$T_{dn} = \frac{\alpha A_n f_u}{\gamma_{m1}}, \quad T_{db1} = \frac{A_{vg} f_y}{\sqrt{3} \gamma_{m0}} + \frac{0.9 A_{tn} f_u}{\gamma_{m1}}, \quad T_{db2} = \frac{0.9 A_{vn} f_u}{\sqrt{3} \gamma_{m1}} + \frac{A_{tg} f_y}{\gamma_{m0}}$$

$$P_d = A_e f_{cd}, \quad P_z = 0.6 V_z^2, \quad V_z = V_b k_1 k_2 k_3$$

$$f_{cd} = \chi \frac{f_y}{\gamma_{m0}}, \quad \chi = \frac{1}{\phi + \sqrt{\phi^2 - \lambda_e^2}}, \text{ where } \phi = 0.5 \left[1 + \alpha (\lambda_e - 0.2) + \lambda_e^2 \right]$$

$$\lambda_e = \sqrt{k_1 + k_2 \lambda_{vv}^2 + k_3 \lambda_\phi^2}$$

$$\text{where } \lambda_{vv} = \frac{\left(\frac{l}{r_{vv}} \right)}{\epsilon \sqrt{\frac{\pi^2 E}{250}}} \text{ and } \lambda_\phi = \frac{(b_1 + b_2) / 2t}{\epsilon \sqrt{\frac{\pi^2 E}{250}}}$$

$$t_s = \sqrt{[2.5w(a^2 - 0.3b^2)\gamma_{m0}/f_y]} > t_f$$

Values of χ and f_{cd} (N/mm²) for different values of KL/r_{\min} as per buckling curve 'c'

KL/r_{\min}	10	20	30	40	50	60	70	80	90
χ	1.000	0.987	0.930	0.870	0.807	0.740	0.670	0.600	0.533
f_{cd}	227	224	211	198	183	168	152	136	121
KL/r_{\min}	100	110	120	130	140	150	160	170	180
χ	0.471	0.416	0.368	0.327	0.291	0.261	0.234	0.212	0.192
f_{cd}	107	94.6	83.7	74.3	66.2	59.2	53.3	48.1	43.6