

(ISO/IEC - 27001 - 2013 Certified)

Model Answer: Winter - 2019

Subject: Mechanics of Structures

Sub. Code: 22303

Important Instructions to examiners:

- 1) The answers should be examined by key words and not as word-to-word as given in the model answer scheme.
- 2) The model answer and the answer written by candidate may vary but the examiner may try to assess the understanding level of the candidate.
- 3) The language errors such as grammatical, spelling errors should not be given more importance. (Not applicable for subject English and Communication Skills.)
- 4) While assessing figures, examiner may give credit for principal components indicated in the figure. The figures drawn by the candidate and those in the model answer may vary. The examiner may give credit for any equivalent figure drawn.
- 5) Credits may be given step wise for numerical problems. In some cases, the assumed constant values may vary and there may be some difference in the candidate's answers and the model answer.
- 6) In case of some questions credit may be given by judgment on part of examiner of relevant answer based on candidate's understanding.
- 7) For programming language papers, credit may be given to any other program based on equivalent concept.

Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.1		Attempt any <u>FIVE</u> of the following:		(10)
	(a)	Define Hooke's law with expression.		
	Ans.	Hook's law.	1	
		It states that when a material is loaded within its elastic limit, the		
		stress produced is directly proportional to the strain.		
		σαε	1	2
		$\frac{\sigma}{e} = \text{Constant} = E$		
	(b) Ans.	Write down formula of M-I of quarter circle about its centroidal axes.		
		M.I. of quarter circle $(I_{XX}) = 0.055R^4$	1	
		M.I. of quarter circle $(I_{YY}) = 0.055 R^4$	1	2
	(c) Ans.	Define modulus of rigidity and bulk Modulus. Bulk Modulus (K) : When a body is subjected to three mutually perpendicular like stresses		
		of same intensity then the ratio of direct stress and the corresponding volumetric strain of the body is constant and is known as Bulk Modulus.	1	
		Modulus of rigidity (G):		
		It is ratio of shear stress to shear strain, is called as Modulus of Rigidity.	1	2



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Q.1				
	(d)	Define stress and strain.		
	Ans.	Stress: The internal resistance force against the deformation per unit	1	
		cross sectional area is called stress.		
		Strain: When a body of an elastic material is subjected to an axial	1	2
		force it undergoes change in dimensions. The change in dimension per	1	2
		original dimension is called as strain.		
	(e)	Write Euler's and Rankine's formula with meaning of each term.		
	Ans.	Euler's formula,		
		$P_E = \frac{\pi^2 E I_{\min}}{L_c^2}$	1	
		e	1	
		Where,		
		$P_E = Euler's$ buckling load at failure.		
		E = Modulus of elasticity of column material.		
		I_{min} = Minimum moment of inertia of column section.		
		Le = Effective length of the column.		
		Rankine's Formula,		
			1	2
		$P_R = \frac{\sigma_c A}{1 + \alpha \lambda^2}$		
		Where,		
		$P_R = Rankine's$ buckling load at failure.		
		σ_c = Crushing Stress.		
		A= Cross sectional area of column.		
		a= Rankine's constant.		
		λ = Slenderness ratio.		
	(P)	Define shear force and bending moment.		
	(f)	Shear force: Shear force at any cross section of the beam is the	1	
	Ans.	algebraic sum of all vertical forces on the beam acting on right side or	1	
		left side of the section is called as shear force.		
		OR		
		A shear force is the resultant vertical force acting on the either side of		
		a section of a beam.		
		Bending Moment: Bending moment at any section at any cross		
		section is the algebraic sum of the moment of all forces acting on the	1	2
		right or left side of section is called as bending moment.	1	2



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Que. No.	Sub. Que.	Model Answer	Marks	Total Mark
Q.1	(g) Ans.	Give relation between average and maximum shear stress for rectangular and circular cross section. 1. Rectangular Section: $q_{max} = \frac{3}{2} q_{avg}$	1	
		2. Circular Section: $q_{\text{max}} = \frac{4}{3} q_{avg}$	1	2



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Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.2		Attempt any <u>THREE</u> of the following:		(12)
	(a)	State the parallel axis theorem and perpendicular axis theorem.		
	Ans.	Parallel axis theorem: It states that the M. I. of a plane section about any axis parallel to the centroidal axis is equal to the M. I. of the section about the centroidal axis plus the product of the area of the section and the square of the distance between the two axes.	2	
		Perpendicular axis theorem: It states MI of a plane lamina about an axis perpendicular to the plane of lamina and passing through the centroid of the lamina is equal to the addition of the moments of inertia of the lamina about its centroidal axes.	2	4
	(b)	Determine M-I about both axes for a Hollow rectangular section having 150 mm width and 90 mm depth.		
		Note		
		The inner dimensions of hollow rectangular section are not given.		
		Therefore assume inner dimensions as follows.		
		Width $(b)=110 \text{ mm and Depth } (d) = 50 \text{ mm}$		
		(If students assumed the appropriate dimensions and try to attempt should be considered.)		
	Ans.	Data: B=150mm, D = 90mm, b=110mm, d=50mm.		
		Calculate: MI about both axis		
		$\begin{array}{c} \mathbf{y} \\ \mathbf{y} \\ \mathbf{y} \\ \mathbf{y} \\ \mathbf{y} \\ \mathbf{y} \\ \mathbf{y} \end{array}$		
		$I_{XX} = \left(\frac{BD^3}{12} - \frac{bd^3}{12}\right) = \left(\frac{150 \times 90^3}{12} - \frac{110 \times 50^3}{12}\right) = 79666666.67 = 7.967 \times 10^6 mm^4$	2	
		$I_{YY} = \left(\frac{DB^3}{12} - \frac{db^3}{12}\right) = \left(\frac{90 \times 150^3}{12} - \frac{50 \times 110^3}{12}\right) = 197666666.67 = 19.77 \times 10^6 mm^4$	2	4



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Q.2	(c)	Calculate the moment of inertia of a L- section about the XX axis passing through the center of gravity for a section as shown in fig. No. 1.		
		$ \begin{array}{c} \xrightarrow{10} \text{mm} \leftarrow \\ & & & \\ & & \\ & & \\ & & \\ & & & \\ & & \\ & & & \\ & & \\ & & & \\ & & $		
	Ans.	$a_{1} = 150 \times 10 = 1500 \ mm^{2} \qquad y_{1} = \frac{150}{2} = 5mm$ $a_{2} = 10 \times 140 = 1400 \ mm^{2} \qquad y_{2} = 10 + \frac{140}{2} = 80mm$		
		$\overline{y} = \frac{a_1 y_1 + a_2 y_2}{a_1 + a_2} = \frac{(1500 \times 5) + (1400 \times 80)}{1500 + 1400} = 41.21 \text{mm from the base.}$	1	
		$I_{xx} = I_{xx_1} + I_{xx_2} = (I_G + ah^2)_1 + (I_G + ah^2)_2$ $I_{xx} = \left(\frac{bd^3}{12} + ah^2\right)_1 + \left(\frac{bd^3}{12} + ah^2\right)_2$	1	
		$I_{xx} = \left(\frac{150 \times 10^{3}}{12} + \left(1500 \times (41.21 - 5)^{2}\right)\right)_{1} + \left(\frac{10 \times 140^{3}}{12} + \left(1400 \times (80 - 41.21)^{2}\right)\right)_{2}$ $I_{xx} = (1979246.15)_{1} + (4393196.407)_{2}$	1	
		$I_{xx} = 6372442.557 mm^4$	1	4
	(d)	Calculate the M-I @ YY axis for following section.		
		$\begin{array}{c} 100 \text{ mm} \\ \hline \\ $		



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Q.2	(d) Ans.	i) Calculation of X: $A_1 = 100 \times 10 = 1000 \text{ mm}^2$ $A_2 = 180 \times 8 = 1440 \text{ mm}^2$ $A_3 = 100 \times 10 = 1000 \text{ mm}^2$ $X_1 = 46 + \frac{100}{2} = 96 \text{ mm},$ $X_2 = 46 + \frac{8}{2} = 50 \text{ mm},$ $X_3 = 50 \text{ mm},$ $X = \frac{A_1 X_1 + A_2 X_2 + A_3 X_3}{A_1 + A_2 + A_3} = \frac{(1000 \times 96) + (1440 \times 50) + (1000 \times 50)}{1000 + 1440 + 1000} = 63.37 \text{ mm}$ ii) Calculation of I_{xx} :	1	
		Here, $h_1 = X_1 - X = 96-63.37 = 32.63 \text{ mm}$ $h_2 = \dot{X} - X_2 = 63.37 - 50 = 13.37 \text{ mm}$ $h_3 = \dot{X} - X_3 = 63.37 - 50 = 13.37 \text{ mm}$ $I_{yy} = I_{yy1} + I_{yy2} + I_{yy3}$ $I_{yy} = (I_6 + Ah^2)_1 + (I_6 + Ah^2)_2 + (I_6 + Ah^2)_3$ $I_{yy} = (\frac{bd^3}{12} + Ah^2)_1 + (\frac{bd^3}{12} + Ah^2)_2 + (\frac{bd^3}{12} + Ah^2)_3$ $I_{yy} = (\frac{10 \times 100^3}{12} + 1000 \times 32.63^2) + (\frac{180 \times 8^3}{12} + 1440 \times 13.37^2) + (\frac{10 \times 100^3}{12} + 1000 \times 13.37^2)$ $\overline{I_{yy} = 3.175 \times 10^6 \text{ mm}^4}$	1 1	4



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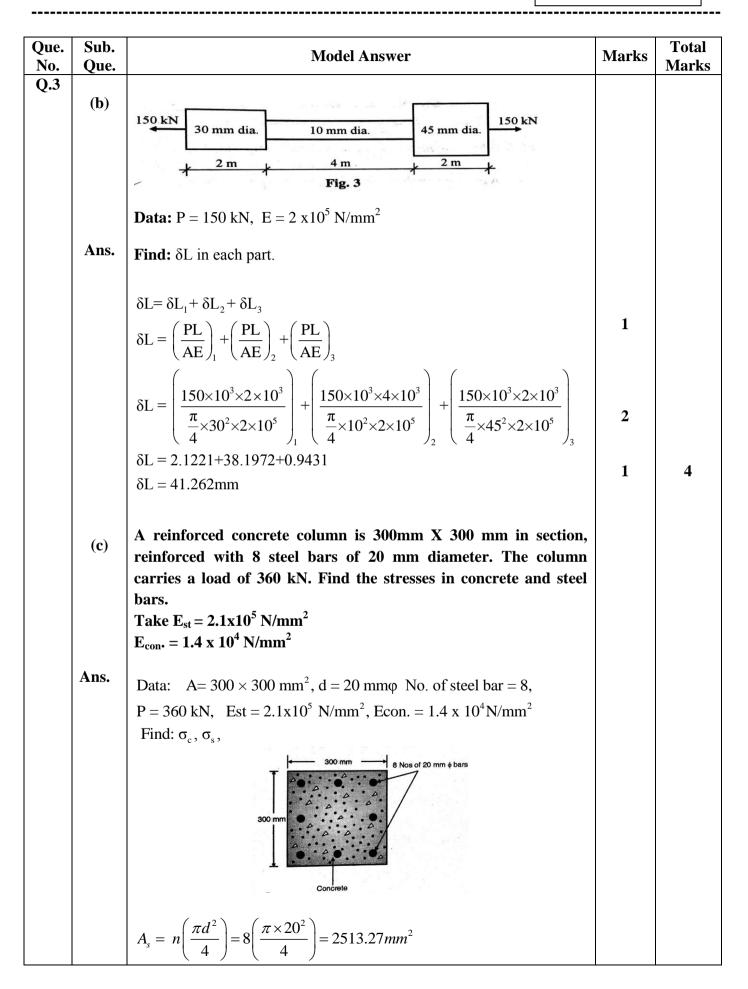
Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.3		Attempt any <u>THREE</u> of the following :		(12)
	(a)	A steel rod 20 mm in diameter 1.2 m long is heated through 120° C at the same time subjected to a pull 'P' if the total extension of the rod is 3 mm calculate the magnitude of 'P'. Take $\alpha = 12 \times 10^{-6} / \circ$ C and E= 200GPa.		
	Ans.	Data : d =20 mm, L = 1.2 m, T= 120°C, , E= 2 x 10^5 N/mm ² and $\alpha_S = 12$ x 10^{-6} / ° C Find: P=?		
		$A = \frac{\pi d^2}{4} = \frac{\pi \times 20^2}{4} = 314.16 mm^2$		
		<i>i</i>) δL_1 due to change in temperature.		
		$\delta L_1 = L \times \alpha \times T$	1	
		$\delta L_1 = 1200 \times 10^3 \times 12 \times 10^{-6} \times 120$ $\delta L_1 = 1.728 mm$		
		<i>ii</i>) δL_2 due to force applied.		
		$\delta L_2 = \frac{PL}{AE}$		
		$\delta L_2 = \frac{P \times 1200}{314.16 \times 200 \times 10^3}$	1	
		$\delta L_2 = (1.91 \times 10^{-5}) P mm$		
		iii) Total change in length is δL .	1	
		$\delta L = \delta L_1 + \delta L_2$		
		$3 = 1.728 + (1.91 \times 10^{-5})P$ P = 66598.82 N	1	4
		$P = 66.60 \ kN$		-
	(b) Ans.	A bar having cross-section as given in fig. No. 3 is subjected to a tensile load of 150 kN. Calculate the change in length of each part along with the total change in length if $E = 2 \times 10^5$ N/m.		
		along with the total change in length if $E = 2 \times 10^{-10/10}$.		



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~	Sub. Que.	Model Answer	Marks	Total Marks
Q.3	(c)	$A_{c} = A_{g} - A_{s}$ $A_{c} = 300 \times 300 - 2513.27$ $A_{c} = 87486.72mm^{2}$ $\frac{\sigma_{s}}{\sigma_{c}} = m$ $\frac{2.1 \times 10^{5}}{1.4 \times 10^{4}} = 15$ $\sigma_{s} = m \times \sigma_{c}$ $\sigma_{s} = 15\sigma_{c}$ $P = P_{s} + P_{c}$ $P = \sigma_{s}A_{s} + \sigma_{c}A_{c}$ $360 \times 10^{3} = (15\sigma_{c})2513.27 + \sigma_{c}87486.72$ $360 \times 10^{3} = (37699.11 + 87486.72)\sigma_{c}$ $\boxed{\sigma_{c} = 2.876N/mm^{2}}$ $\sigma_{s} = 15\sigma_{c}$ $\sigma_{s} = 15 \times 2.876$	1 1 1 1	4
	(d)	$\sigma_s = 43.136N / mm^2$ A Circular bar of diameter 25 mm and 3.5 m long is subjected to a tensile load of 40 kN. Shows an elongation of 60mm. Determine stress, strain and modulus of elasticity.		
	Ans.	Data: d=25 mm, L=3.5 m, P= 40 kN, $\delta L = 60 \text{ mm}$ Find: σ , e, E=? $\sigma = \frac{P}{A} = \frac{40 \times 10^3}{\frac{\pi}{4} \times 25^2} = 81.487 \text{ N/mm}^2$ $e = \frac{\delta L}{L} = \frac{60}{3.5 \times 10^3} = 0.01714$ $E = \frac{\sigma}{e} = \frac{81.487}{0.01714} = 4753.43 \text{ N/mm}^2$	1 1 2	4



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Q.4	Que.	Attempt any <u>THREE</u> of the following :		(12)
	(a)	For a given material E =110 GPa, G = 43 GPa find K and μ . Data: E=110GPa, G= 43GPa Find: K=?, μ =?		
	Ans.	$E = 2G (1+\mu)$ 110 = 2×43×(1+ μ)	1	
		$\mu = 0.279$	1	
		$E = 2K (1-2\mu)$ 110 = 2K (1-2×0.279)	1	
		$K = 82.982 \ GPa$	1	4
	(b)	In a biaxial stress system, the stresses along the two directions are the $\sigma_x=50 \text{ N/mm}^2$ and $\sigma_y=30 \text{ N/mm}^2$ both tensile. Determine the strains along these two directions. E = 2 x 10 ⁵ N/mm ² and Poisson's ratio=0.3.		
	Ans.	Data: $\sigma x=50 \text{ N/mm}^2$, $\sigma y=30 \text{ N/mm}^2$ b=30mm, E=2 x 10 ⁵ N/mm ² , $\mu=0.3$		
		Find: e_x , $e_y=?$		
		$\sigma_y = 30 \text{ N/mm}^2$		
		$\sigma_{\rm x} = 50 \text{ N/mm}^2$ $\sigma_{\rm x} = 50 \text{ N/mm}^2$		
		$\sigma_y = 30 \text{ N/mm}^2$		



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Q.4	(b)	$e_{x} = \frac{\sigma_{x}}{E} - \mu \frac{\sigma_{y}}{E} = \frac{1}{E} \left(\sigma_{x} - \mu \sigma_{y} \right)$	1	
	Ans.	$e_{x} = \frac{1}{2 \times 10^{5}} (50 - (0.3 \times (30)))$ $e_{x} = 20.5 \times 10^{-5}$ $e_{y} = \frac{\sigma_{y}}{E} - \mu \frac{\sigma_{x}}{E} = \frac{1}{E} (\sigma_{y} - \mu \sigma_{x})$	1	
		$e_{y} = \frac{1}{2 \times 10^{5}} ((30) - (0.3 \times 50))$ $e_{y} = 7.5 \times 10^{-5}$	1	4
	c)	State the relation between E, G and K with expressions.		
	Ans.	$E = 3K (1 - 2\mu)$ $E = 2G (1 + \mu)$ Where, E = Young's Modulus G = Modulus of Rigidity K = Bulk Modulus $\mu = \text{Poisson's Ratio}$ $E = 3K \left[1 - 2 \left(\frac{E}{2G} - 1 \right) \right]$ $\left[- \left(E - 1 \right) \right]$	1	
		$E = 3K \left[1 - \left(\frac{E}{G} + 2\right) \right]$ $E = 3K \left[3 - \frac{E}{G} \right]$ $E = 3K \left(\frac{3G - E}{G} \right)$ $EG = 3K (3G - E)$ $EG = 9KG - 3KE$	2	4



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Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.4	(d)	Draw SF and BM diagram for the cantilever beam as shown in fig. No. 4.		WIALKS
		$A = \begin{bmatrix} 20 \text{ kN} & 20 \text{ kN} \\ 10 \text{ kN/m} & 10 \text{ kN/m} \\ 1 \text{ m} & B & 2 \text{ m} & C \\ 3 \text{ m} & & & \\ \hline & & & & \\ \hline & & & & \\ \hline & & & &$		
	Ans.	I) Reaction Calculation: $\sum Fy = 0$ $RA = 20+20+10\times3 = 70kN$		
		II) SF Calculation: A = +70kN $B_L = +70-10 \times 1=60kN$ $B_R = +60-20=+40kN$ $C_L = +40-20=+20kN$ C = +20-20=0kN (ok)	1	
		III) BM Calculation: C = 0 (B is Free end) $B = -20 \times 2 - (10 \times 2 \times 1) = -60$ kN-m $A = -20 \times 3 - 20 \times 1 - (10 \times 3 \times 1.5) = -125$ kN-m	1	

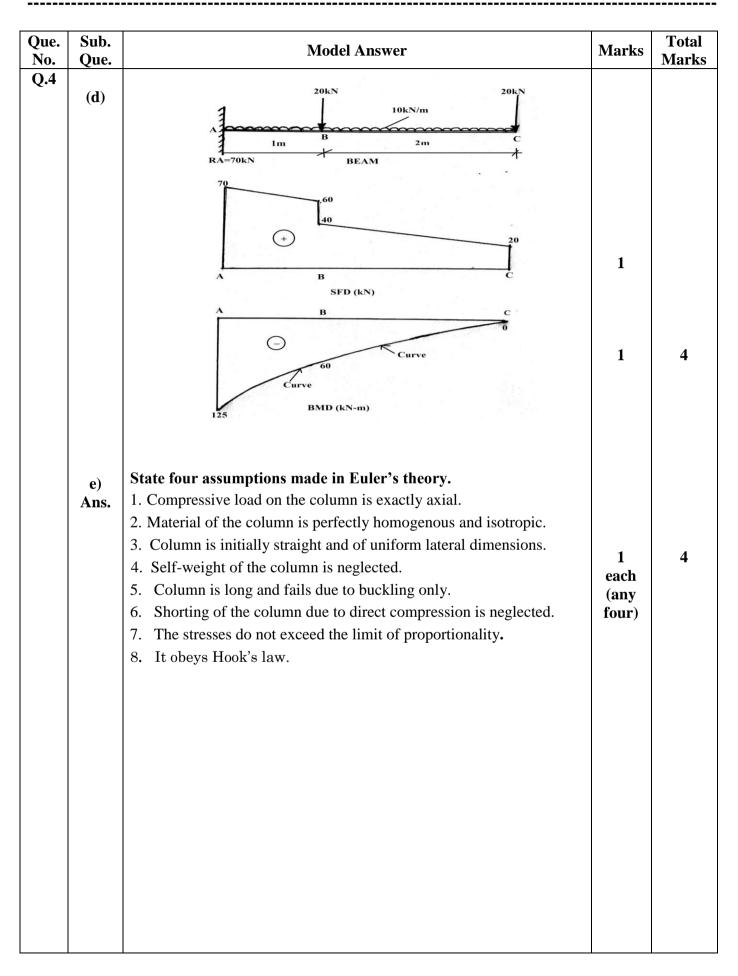


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Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.5	Zuci	Attempt any <u>TWO</u> of the following :		(12)
	(a)	Draw shear force and bending moment for beam as shown in Fig. No. 5 50 kN $60 kN$ $15 kN/mA \xrightarrow{20 \text{ kN/m}} 1.5 \text{ m} \xrightarrow{D} 1$		
		(Note: If students assume any other value of point load and try to attempt should be considered.)		
	Ans.	L Departion Coloulation		
		I. Reaction Calculation: $\sum M_{A} = 0$		
		$\boxed{R_B \times 4.5 = (20 \times 1.5) \times \frac{1.5}{2} + (30 \times 1.5) + (60 \times 3) + \left[(15 \times 1.5) \times \left(3 + \frac{1.5}{2}\right)\right]}$		
		$R_{B} = \frac{22.5 + 45 + 180 + 84.375}{4.5}$		
		$R_B = 73.75 \ kN$	1	
		$\sum F_{Y} = 0$		
		$R_A + R_B = (20 \times 1.5) + 30 + 60 + (15 \times 1.5)$		
		$R_A + R_B = 30 + 30 + 60 + 22.5 - 73.75$ $R_A = 68.75 \ kN$		
		II. SF Calculation:		
		$SF at A = +68.75kN$ $C_L = +68.75 \cdot (20 \times 1.5) = +38.75kN$ $C_R = +38.75 \cdot 30 = +8.75kN$	1	
		$D_L = +8.75kN$		
		$D_R = +8.75-60 = -51.25kN$ $B_L = -51.25 - (15x1.5) = -73.75kN$ $B = -73.75 - 73.75 = 0 \qquad (\Box \ ok)$		



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Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.5	(a)	III. BM Calculation:		
		BM at A and $B = 0$ (Supports A and B are simple)		
		$C = + 68.75 \times 1.5 - 20 \times 1.5 \times \frac{1.5}{2} = + 80.625 kN - m$	1	
		$D = 73.75 \times 1.5 - 15 \times 1.5 \times \frac{1.5}{2} = + 93.75 kN - m$	1	
		30 kN 60 kN		
		$A \xrightarrow{20 \text{ kN/m}} B$ $C \xrightarrow{D} 1.5 \text{ m} \xrightarrow{-1.5 \text{ m}} $		
		RA=68.75kN Beam RB=73.75kN		
		68.75		
		38.75		
		€ 8.75 8.75	1	
		51.25 ⊙		
		SFD in kN 73.75		
		93.75		
		€		
			1	6
		BMD in kN.m		



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	Que.	Model Answer	Marks	Marks
<u>No.</u> Q.5	(b)	Draw S.F. and B.M. diagram for overhanging beam as shown in		
		fig. No. 6.		
		50 kN		
		30 kN/m		
		A		
		4 m $1 m$		
	Ans.	Fig. 6		
	Alls.	I. Support Reactions:		
		$\Sigma M_A = 0$	1	
		$R_B \times 4 = (30 \times 5) \times 2.5 + 50 \times 5$		
		$R_{B} = 156.25kN$		
		$\Sigma F_{Y} = 0$		
		$R_A + R_B = (30 \times 5) + 50$		
		$R_A + 156.25 = (30 \times 5) + 50$		
		$R_A = 43.75 kN$		
		II. SF calculations:		
		SF at A = +43.75 kN		
		$B_L = +43.75 - (30 \times 40) = -76.25 \ kN$	1	
		$B_R = -76.25 + 156.25 = +80 \ kN$	T	
		$C_L = + 80 - 30 \times 1 = +50 \ kN$		
		C = +50 - 50 = 0 (ok)		
		III. BM calculations:		
		BM at A and $C = 0$. (:: Supports are simple)		
		$B = -50 \times 1 - 30 \times 1 \times \frac{1}{2} = -65 \ kN - m$	1	
		IV. To calcuate Maximum Bending Moment		
		SF at x = 0,		
	•	$\therefore 43.75 - 30 \times x = 0$		
		$\therefore x = 1.458m from A$		
		$BM_{\rm max} = 43.75 \times 1.458 - 30 \times \frac{1.458^2}{2}$		
		2	1	
		$BM_{\text{max}} = 31.90kN - m$	T	



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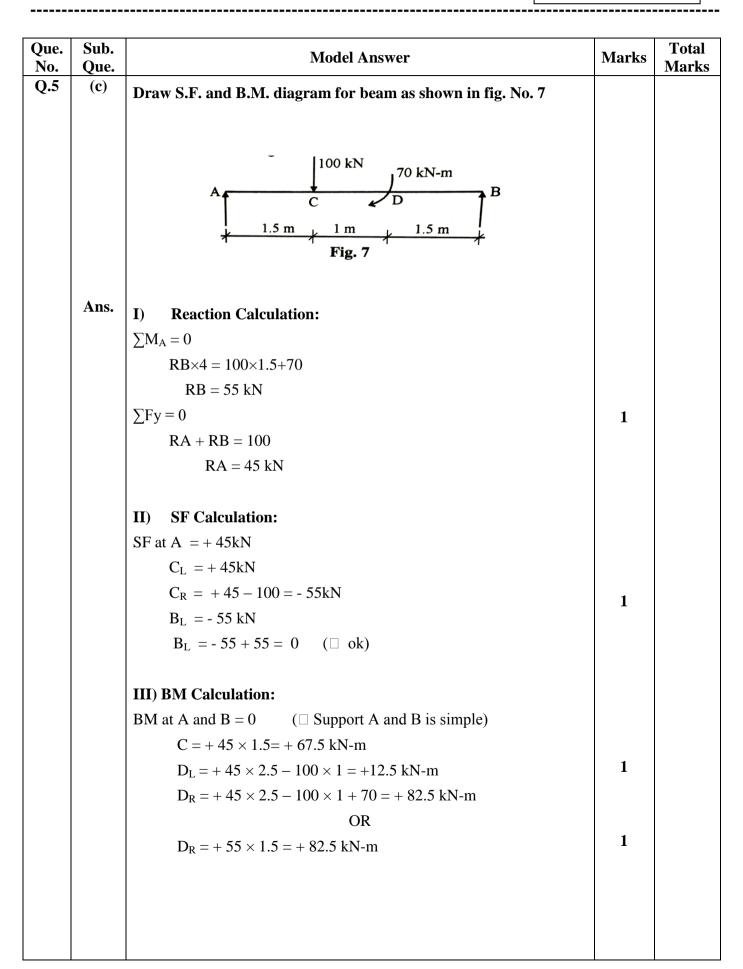
Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.5	(b)	V. To calculate point of contraflexure		
		$At \ dis \tan ce \ X \ BM = 0$		
		$43.75x - 30 \times \frac{x^2}{2}$		
		$x = 2.92 m from \sup port A$		
		30 kN/m $A \xrightarrow{30 \text{ kN/m}} 4 \text{ m} \xrightarrow{B} \xrightarrow{50 \text{ kN}} C$ $A \xrightarrow{R_B} R_B$		
		43.75 kN Point of Contrashear → 50 kN → 1.46m	1	
		SFD in kN 76.25 kN 31.9 kN.m		
		Point of Cotraflexure 2.92m BMD in kN.m 65 kN.m	1	6



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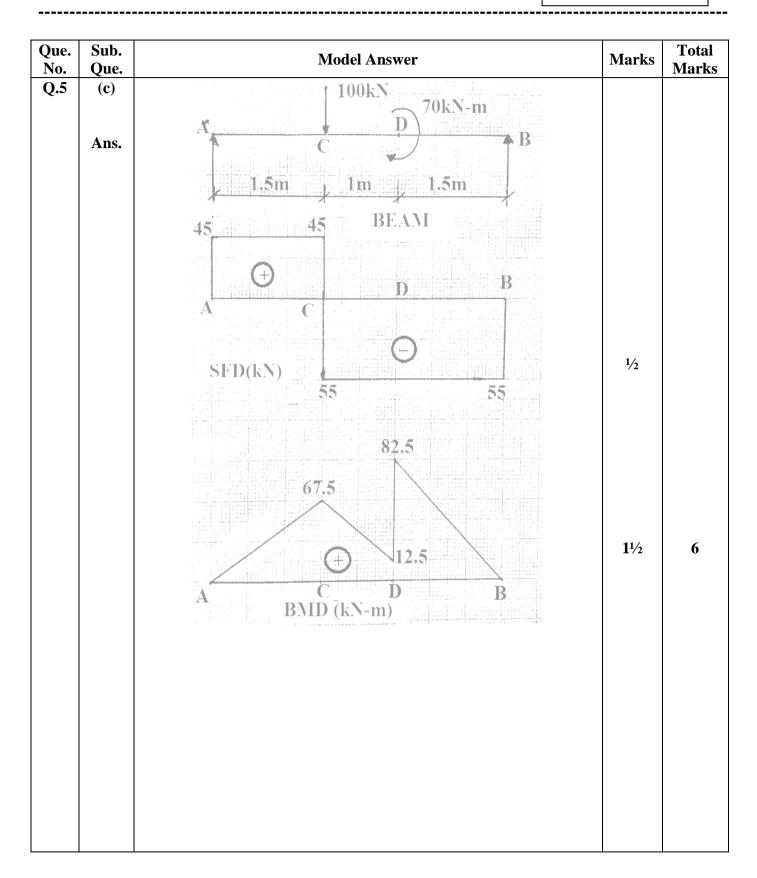




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Q.6		Attempt any TWO of the following :		(12)
	(a)	Solve the following.		
	(i)	Determine by Rankine's formula the safe load on the column of 5.5 m length, with both ends fixed, can carry with a factor of safety 4. The properties of section are A= 1777mm2. Ixx= 11.6x106 mm4. Iyy= $0.84x106$ mm4. $\sigma c = 3200$ N/mm2 and $\alpha = 1/1600$.		
		Given :		
	Ans.	$L = 5.5m, FOS = 4, \sigma_c = 320 N / mm^2, \alpha = \frac{1}{7500},$ $Ixx = 11.6 \times 10^6 mm^4, Iyy = 0.84 \times 10^6 mm^4$		
		As the column is fixed at both ends, effective length is		
		$Le = \frac{L}{2} = \frac{5500}{2} = 2750 \text{ mm}$		
		$Le^{2} = 2$ $K_{\min} = \sqrt{\frac{I_{\min}}{A}} = \sqrt{\frac{0.84 \times 10^{6}}{1777}} = 21.742 \text{ mm}$	1	
		$\lambda_{\min} = \frac{Le}{K_{\min}} = \frac{2750}{21.742} = 126.484$ By $u \sin g$ Rankine's formula,	1	
		$P_{R} = \frac{\sigma_{c} \cdot A}{1 + a\lambda_{\min}^{2}} = \frac{320 \times 1777}{1 + \frac{(126.484)^{2}}{7770}} = 181494.0678N$		
		$Safe \ Load = \frac{P_R}{FOS} = \frac{181494.0678}{4} = 45373.516N = 45.374kN$	1	3



Model Answer: Winter - 2019

Subject: Mechanics of Structures

Sub. Code: 22303

Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.6	(a) (ii)	A simply supported beam has span 7 m carries a point load of 50 kN at the center of the beam. Calculate the modulus of section if bending stress is not to exceed 140 Mpa. With distribution diagram of stress.		
	Ans.	Given: $L = 7m$, $W = 50 \text{ kN}$, $\sigma = 140 \text{MPa}$		
	11115	$M = \frac{WL}{4} = \frac{50 \times 7}{4} = 87.5 \text{ kN} - m = 87.5 \times 10^6 \text{ N} - mm$	1	
		Flexural Equation: $M = \sigma$		
		$\frac{M}{I} = \frac{\sigma}{y}$ $\frac{M}{\sigma} = \left(\frac{I}{y}\right) = Z$		
		$Z = \frac{M}{\sigma} = \frac{87.5 \times 10^6}{140} = 6.25 \times 10^5 mm^3$	1	
		N	1	3
		T 140N/mm ² Bending Stress Distribution Diagram		



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Que.	Sub.	Model Answer	Marks	Total Morks
No. Q.6	Que. (b)	A cantilever is 2 m long and is subjected to an udl of 5 kN/m. The		Marks
Q.0		c/s of a cantilever is a I-section as shown in fig. No. 8. Determine		
		the maximum tensile and compressive stress developed and their		
		position, showing stress distribution diagram.		
		\leftarrow 150 mm \rightarrow 10 mm		
		\uparrow		
		10 mm 90 mm		
		\rightarrow \leftarrow 90 mm		
		< 200 mm →		
	Ans.	Fig. 8		
		i) Calculation of Y :		
		$A_1 = 200 \times 10 = 2000 mm^2$		
		$A_2 = 10 \times 90 = 900 mm^2$		
		$A_3 = 150 \times 10 = 1500 mm^2$		
		$Y_1 = \frac{10}{2} = 5mm$		
		$Y_2 = 10 + \frac{90}{2} = 55mm$		
		$Y_3 = 10 + 90 + \frac{10}{2} = 105mm$		
		$\dot{Y} = \frac{A_1Y_1 + A_2Y_2 + A_3Y_3}{A_1 + A_2 + A_3}$		
		$Y = \frac{(2000 \times 5) + (900 \times 55) + (1500 \times 105)}{2000 + 900 + 1500}$		
		2000 + 900 + 1500		
		Y = 49.32mm		
		$Y_{c} = 49.32mm$	1	
		$Y_T = 110 - 49.32 = 60.68 mm$		



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Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.6	(b)	ii) Calculation of I_{xx} : Here, $h_1 = Y - Y_1 = 49.32 - 5 = 44.32 \text{ mm}$ $h_2 = Y_2 - Y = 55 - 49.32 = 5 \text{ mm}$ $h_3 = Y_3 - Y = 105 - 49.32 = 55.68 \text{ mm}$ $I_{xx} = I_{xx1} + I_{xy2} + I_{xy3}$	1	
		$I_{xx} = (I_{G} + Ah^{2})_{1} + (I_{G} + Ah^{2})_{2} + (I_{G} + Ah^{2})_{3}$ $I_{xx} = \left(\frac{bd^{3}}{12} + Ah^{2}\right)_{1} + \left(\frac{bd^{3}}{12} + Ah^{2}\right)_{2} + \left(\frac{bd^{3}}{12} + Ah^{2}\right)_{3}$ $I_{xx} = \left(\frac{200 \times 10^{3}}{12} + 2000 \times 44.32^{2}\right) + \left(\frac{10 \times 90^{3}}{12} + 900 \times 5.68^{2}\right) + \left(\frac{150 \times 10^{3}}{12} + 1500 \times 55.68^{2}\right)$ $\boxed{I_{xx} = I_{NA} = 9.245 \times 10^{6} \text{mm}^{4}}$	1	
		iii)Bending moment(M): $M = \frac{wL^2}{2} = \frac{5 \times 2^2}{2} = 10 \ kN - m = 10 \times 10^6 \ N - mm$	1	
		<i>iv</i>)Calculation Maximum Stress: $\sigma_{T} = \left(\frac{M}{I_{NA}}\right) \times Y_{T} = \left(\frac{10 \times 10^{6}}{9.245 \times 10^{6}}\right) \times 60.68 = 65.64 \text{ N} / mm^{2}$ $\sigma_{C} = \left(\frac{M}{I_{NA}}\right) \times Y_{C} = \left(\frac{10 \times 10^{6}}{9.245 \times 10^{6}}\right) \times 49.32 = 53.35 \text{ N} / mm^{2}$	1	
		$\frac{65.64 \text{ MPa}}{y_t = 60.68 \text{ mm}}$ N N N N N N N N N N N N N N N N N N	1	6



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Sub. Code: 22303

Que. No.	Sub. Que.	Model Answer	Marks	Total Marks
Q.6	(c)	A T-section beam having flange 180mm wide and 20 mm thick and web 150 mm long and 20 mm thick carries a udl of 80 kN/m over an effective span of 8 m. Calculate the maximum bending stress.		
	Ans.	$a_1 = 20 \times 150 = 3000 \text{ mm}^2 y_1 = \frac{150}{2} = 75 \text{ mm}$ $a_2 = 180 \times 20 = 3600 \text{ mm}^2 y_2 = 150 + \frac{20}{2} = 160 \text{ mm}$		
		$\overline{y} = \frac{a_1 y_1 + a_2 y_2}{a_1 + a_2} = \frac{(3000 \times 75) + (3600 \times 160)}{3000 + 3600} = 121.36 \text{ mm from the base.}$ $y_c = 48.64 \text{ mm}, y_t = 121.36 \text{ mm}$ $I_{xx} = I_{xx_1} + I_{xx_2} = (IG + ah^2)_1 + (IG + ah^2)_2$ $I_{xx} = \left(\frac{bd^3}{12} + ah^2\right)_1 + \left(\frac{bd^3}{12} + ah^2\right)_2$	1	
		$I_{xx} = \left(\frac{20 \times 150^{3}}{12} + \left(3000 \times (121.75 - 75)^{2}\right)\right)_{1} + \left(\frac{180 \times 20^{3}}{12} + \left(3600 \times (48.64 - 10)^{2}\right)\right)_{2}$ $I_{xx} = (12072748.8)_{1} + (5494978.56)_{2}$ $I_{xx} = 17567727.36 \text{mm}^{4} = 17.568 \times 10^{6} \text{mm}^{4}$	1	
		Maximum Bending moment : $(M) = \frac{wL^2}{8} = \frac{80 \times 8^2}{8} = 640 \ kN - m = 640 \times 10^6 \ N - mm$ Maximum stress : $\sigma_c = \frac{M}{I} \times y_t = \frac{640 \times 10^6}{17.568 \times 10^6} \times 48.64 = 1771.976 \ N / mm^2(C)$	1	
		$\sigma_{t} = \frac{M}{I} \times y_{c} = \frac{640 \times 10^{6}}{17.568 \times 10^{6}} \times 121.36 = 4421.198N / mm^{2}(T)$ $\overline{\sigma_{t} = \sigma_{\text{max}} = 4421.198N / mm^{2}(T)}$	1	6
		(Note- If students assume a cantilever type of beam and try to attempt should be considered).		